

Fuzzy Gain Scheduling of PID (FGS-PID) for Speed Control Three Phase Induction Motor Based on Indirect Field Oriented Control (IFOC)

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Abstract

This paper propose about using PID control system based on K_p , K_i , and K_d parameter determination with scheduling process from fuzzy logic. Control system is used to arrange speed of three phase induction motor using IFOC method. This method can be minimized the main problem from speed control of induction motor which is a transient condition. The robustness validation from this system use testing process of dynamic speed which is compared with the other control system to know the system performance in transient condition such as (rise time, overshoot, undershoot and settling time). The result shows using the proposed system has better performance responses which is requiring 0.001 seconds time in transient condition up to steady state condition without overshoot and undershoot problem.

Keywords: PID, Fuzzy scheduling, IFOC, Induction Motor, and Performance Control.

1. INTRODUCTION

Nowadays, like a consequence of the important progress in the power electronics and of microcomputing, the control of the AC electric machines known a considerable development and a possibility of the real time implantation applications. It is widely recognized that the induction motor is going to be the main actuator for industrial purposes [1], [2]. Indeed, as compared to the DC machine, it provides a better power or mass ratio, a simpler maintenance and relatively lower cost. However, it is traditionally for a long time, used in industrial applications that do not require high performances, this because its control is a more complex problem, its high nonlinearity and its high coupled structure. Furthermore, the motor parameters are time-varying during the normal operation and most of the state variables are not measurable. On the other hand, the direct current

(D.C) machine was largely used in the field of the variable speed applications, where torque and flux are naturally decoupled and can be controlled independently by the torque producing current and the flux producing current. Since Blashke and Hasse have developed the new technique known as vector control [1-4], the use of the induction machine becomes more and more frequent. This control strategy can provide the same performance as achieved from a separately excited DC machine, and is proven to be well adapted to all type of electrical drives associated with induction machines[5].The vector control technique has been widely used when high performance rotary machine drive is required, especially the Indirect Field Oriented Control (IFOC) that is the most effective vector control of three phase induction motor due to the simplicity of designing and implementation [6]. Decoupled torque and flux control in IFOC of induction machines permits high dynamic response. While, induction motor control can't apart from its previous condition. The real nonlinear characteristic from motor and the modification parameter from control caused to the modification value in control process when the time of transient condition was toward to the steady state in set point achievement. Using appropriate control system can be minimized its problem.

The most widely used controller in the industrial applications is the PID-type controllers because of their simple structures and good performances in a wide range of operating conditions [7]. In the literature, the PID controllers can be divided into two main parts: In the first part, the controller parameters are fixed during control operation. These parameters are selected in an optimal way by known methods such as the Zeigler and Nichols, poles assignment...etc. The PID controllers of this part are simple but cannot always effectively control systems with changing parameters or have a strong nonlinearity; and may need frequent on-line retuning [8]. In the second part, the controllers have an identical structure to PID controllers but their parameters are tuned on-line based on parameters estimation of the process. Such controllers are known as adaptive PID controllers [2]. The application of knowledge-based systems in process control is growing, especially in the field of fuzzy control [9-12]. In fuzzy control, linguistic descriptions of human expertise in controlling a process are represented as fuzzy rules or relations. This knowledge base is used by an inference mechanism, in conjunction with some knowledge of the states of the process (say, of measured response variables) in order to determine control actions. Although they do not have an apparent structure of PID controllers, fuzzy logic controllers may be considered nonlinear PID controllers whose parameters can be determined on-line based on the error signal and their time derivative or difference [11].

This paper proposed the application FGS-PID for speed control of three phase induction motor based on IFOC. The new scheme utilizes fuzzy rules and reasoning to determine the controller parameters, and the PID controller generates the control signal for the process on IFOC systems. It is

demonstrated in this paper that human expertise on PID gain scheduling can be represented in fuzzy rules. Furthermore, better control performance can be expected in the proposed method than that of the PID controllers with fixed parameters on dynamic conditions. The investigation of transient condition (involve rise time, overshoot, undershoot, and settling time) in speed of dynamic is presented section 2. The comparison between FGS-PID and other control is presented section 3.

2. RELATED WORKS

The theory of Fuzzy Gain Scheduling-PID was firstly developed by Zhen-Yu Zhao, Masayoshi Tomizuka, and Satoru Isaka in 1993. Using Fuzzy gain scheduling could be used to determine gain parameters of PID control. PID is one of popular control in industrial because it has simple design, robust control and also easy to be implemented. However, parameter of gain PID is difficult to be determined which needs re-tuning to get a good result. One of developed tuning methods is Ziegler Nichols that is simple in determining of K_p gain, K_i , and K_d of PID parameters [7].

Fuzzy logic was presented by Prof. L. Zadeh in 1965 from California University. Fuzzy logic was founded after crisp logic method. The value of crisp logic is true "1" or false "0". Fuzzy logic has uncertain value between true and false. Fuzzy logic allows membership value between 0 and 1 and also several variables that are expressed in linguistic language such as positive, zero, and negative. The principle of FGS-PID is using two inputs (error and Δ -error) with output fuzzy k_p' , k_d' , and α . Fuzzy k_p' is used to schedule parameter gain (p), k_d' is used to schedule parameter gain (T_d), and α is used to schedule gain (T_i). By applying gain system scheduling of PID parameter, PID tuning process is easier to do in stable or unstable condition. In Zhao and friends' presentation, also comparing the output response system of FGS-PID control, PID-ZN, and Kitamori. The comparisons are done from output control system for second, third, and fourth order. The result shows that FGS-PID has more optimal response because it can reduce overshoot condition and oscillation system [13].

Then, Bousserhane presents optimal fuzzy gains scheduling of PI controller for induction motor speed control. To overcome the disadvantages of PID controllers and FLC, we propose in this paper a combination between them together. PID parameters controller can be tuned on-line by an adaptive mechanism based on a fuzzy logic for induction machine speed control. Design of an optimal fuzzy gain scheduling of PI controller combines the merits of the sliding mode control and the fuzzy inference mechanism is proposed. A fuzzy gain scheduling of conventional PI controller is investigated, in which the fuzzy logic system is used on-line to generate the PI controller parameters [2].

In this paper, it will be proposed design about speed control of three-phase induction motor based on IFOC with combining PID controller and Fuzzy as gain scheduling parameter of k_p , k_i , and k_d that can simplify the

tuning process of PID control to get a better response result in transient condition at speed of dynamic.

3. ORIGINALITY

The contribution of this paper is to implement speed control of induction motor based on PID with scheduling and reasoning from fuzzy logic control to obtain parameter system which is suitable with determined condition using IFOC method. Using the proposed method can be minimized the problem of induction motor rotation in transient condition which has non-linear characteristic. The principle of fuzzy gain scheduling is used to arrange the PID gain that is appropriate with the declared condition. The output of control system is control signal which is used for IFOC system in control of induction motor system. The implementation of proposed IFOC method is simply to apply which is using control system based on vector technique. The vector technique is oriented to the field control which can be controlled the torque unit and flux separately. This system is usually called by decoupled system. the modification of flux and torque can be influenced to the motor rotation which is represented as current and speed modification.

The parameter modification from control system can be decreased the performance of control system which is showed from motor responses in transient condition. Using FGS-PID is one of solution to minimize this problem. The control design is arranged for 0 – 1000 Rpm speed which can be given the better result in modification parameter condition. Verification process and the robustness test of this system is used dynamic speed control system which is observed in transient condition involve rise time, overshoot, undershoot and time settling.

4. SYSTEM DESIGN

4.1 RESEARCH METHOD

4.1.1 PID Controller

PID control is a combination from three methods; those are proportional control, integral, and derivative. Combination of these methods can be used to minimize disadvantage of each controls. Proportional control (P) has function to accelerate up to set point condition, but it can cause overshoot. Disadvantage of control (P) can be solved by adding integral control (I) that functions to reduce overshoot, but system will be slow. So it needs derivative control (D) to accelerate system. But sometimes, it causes oscillation condition before getting steady state. The equation of PID control is given to this following equation [13]:

$$u(t) = K_p e(t) + K_i \int_0^t e(t) + K_d \frac{d}{dt} e(t) \quad (1)$$

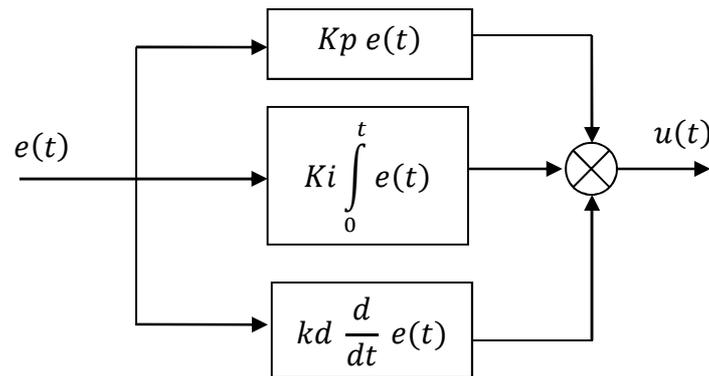


Figure 1. Blok of diagram PID controller

PID control has gain parameters that can be influenced to the control; those are K_p , K_i , and K_d . The values of gains can be used to get a good control result. However, it is difficult to be determined that needs re-tuning to get a good result. Ziegler-Nichols (ZN) method is one solution to determine a difficult a gain value of good control. This method also can be used for tuning process.

ZN is one of tuning method that is used for deciding PID parameters. First tuning process is setting K_p , and then set the value of T_i to be unlimited, and set the value of T_d to be zero. Then, increase the value of K_p until the value of oscillation and amplitude are the same. *Gain* that creates oscillation condition is *gain* K_u and oscillation period of full wave is P_u . The value of K_u and P_u are used for getting the value of K_p , K_i , and K_d . ZN tuning rule is shown in table 1 [13].

Table 1. Rule of Ziegler-Nichols Method

Type of Controller	K_p	T_i	T_d
Proportional (P)	$0.5K_u$	-	-
Proportional Integral (PI)	$0.45K_u$	$\frac{P_u}{1.2}$	-
Proportional Integral Derivative (PID)	$0.6K_u$	$\frac{P_u}{2}$	$\frac{P_u}{8}$

4.1.2 Fuzzy gain scheduling-PID

On the Fig 2 shows the PID control system with a fuzzy gain scheduler. The approach taken here is to exploit fuzzy rules and reasoning to generate controller parameters.

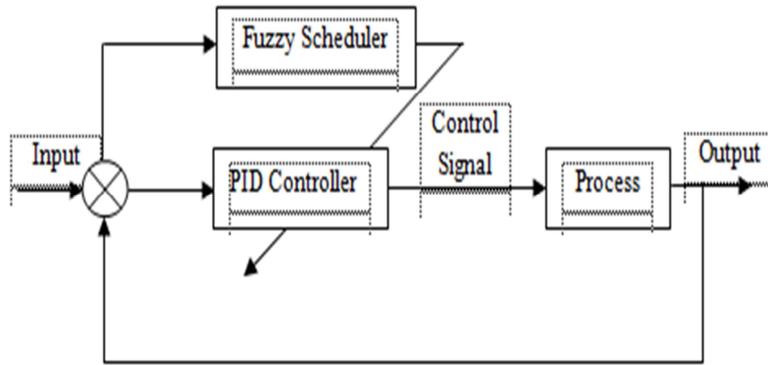


Figure 2. Blok of diagram FGS-PID controller

It is assumed that K_p are in prescribed ranges $[K_p \text{ min}, K_p \text{ max}]$ and $[K_d \text{ min}, K_d \text{ max}]$ respectively. The appropriate ranges are determined experimentally and will be given in equation (4). For convenience, K_p and K_d are normalized into the range between zero and one by the following linear transformation [7]:

$$K_p' = (K_p - K_p \text{ min}) / (K_p \text{ max} - K_p \text{ min}) \tag{2}$$

$$K_d' = (K_d - K_d \text{ min}) / (K_d \text{ max} - K_d \text{ min}) \tag{3}$$

In the proposed scheme, PID parameters are determined based on the current error $e(k)$ and its first difference $\Delta e(k)$. The integral time constant is determined with reference to the derivative time constant and the integral gain is thus obtained by

$$K_i = K_p / (\alpha T_d) = K_p^2 / (\alpha K_d) \tag{4}$$

The parameters K_p' , K_d' , α are determined by a set of fuzzy rules of the form. The membership functions (MF) of these fuzzy sets for error $[e(k)]$ and delta error $[\Delta e(k)]$ are shown in Fig. 3. In this figure, N represents negative, P positive, ZO approximately zero, S small, M medium, B big. Thus NM stands for negative-medium, PB for positive big, and so on.

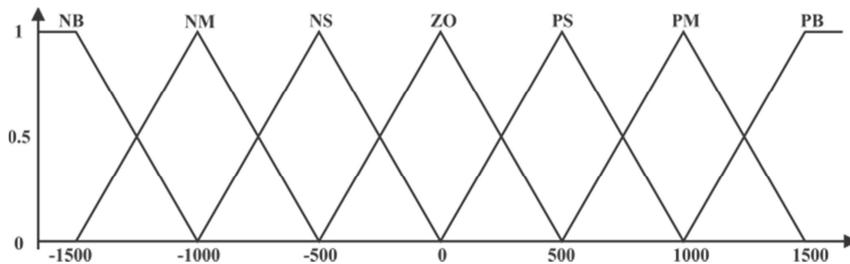


Figure 3. Membership function error and Δ error

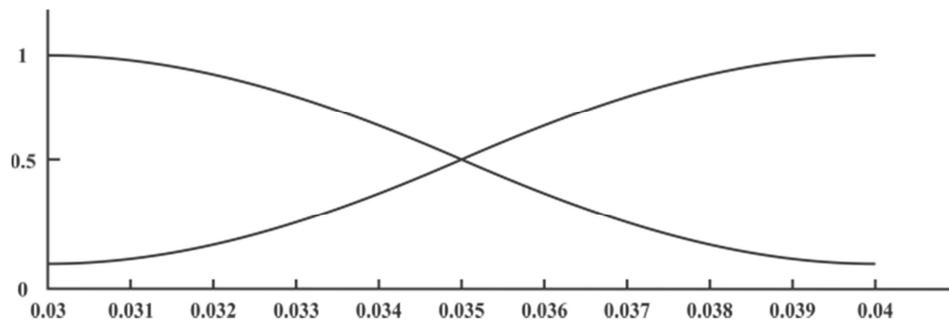


Figure 4. Membership function for K_p' and K_d'

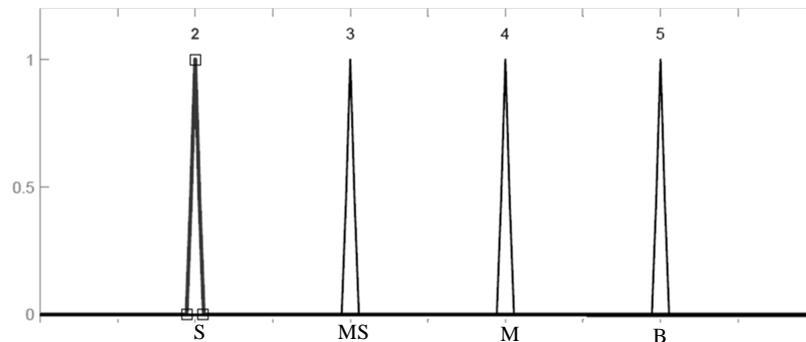


Figure 5. Output of Membership function α

The rule base of Fuzzy gain scheduler to determine PID parameter shown in table 2, 3, and 4 [2].

Table 2. Fuzzy tuning rule for k_p'

		$\Delta error$						
		NB	NM	NS	ZO	PS	PM	PB
e r r o r	NB	B	B	B	B	B	B	B
	NM	S	B	B	B	B	B	S
	NS	S	S	B	B	B	S	S
	ZO	S	S	S	B	S	S	S
	PS	S	S	B	B	B	S	S
	PM	S	B	B	B	B	B	S
	PB	B	B	B	B	B	B	B

Table 3. Fuzzy tuning rule for k_d'

		$\Delta error$						
		NB	NM	NS	ZO	PS	PM	PB
e r r o r	NB	S	S	S	S	S	S	S
	NM	B	B	S	S	S	B	B
	NS	B	B	B	S	B	B	B
	ZO	B	B	B	B	B	B	B
	PS	B	B	B	S	B	B	B
	PM	B	B	S	S	S	B	B
	PB	S	S	S	S	S	S	S

Table 4. Fuzzy tuning rule for α

		$\Delta error$						
		NB	NM	NS	ZO	PS	PM	PB
e r r o r	NB	2	2	2	2	2	2	2
	NM	3	3	2	2	2	3	3
	NS	4	3	3	2	3	3	4
	ZO	5	4	3	3	3	4	5
	PS	4	3	3	2	3	3	4
	PM	3	3	2	2	2	3	3
	PB	2	2	2	2	2	2	2

Based on the result from K_p' , K_d' , α value, PID and FGPS parameter can be calculated using this equation:

$$K_p = (K_{p \max} - K_{p \min}) K_p' + K_{p \min} \tag{5}$$

$$K_p = (K_{p \max} - K_{p \min}) K_p' + K_{p \min} \tag{6}$$

$$K_p^2 / (\alpha K_d) \tag{7}$$

($K_p \max$, $K_p \min$) and ($K_d \max$, $K_d \min$) is obtained from this following equation:

$$K_{p \min} = 0.32 Ku, K_{p \max} = 0.6 Ku \tag{8}$$

$$K_{d \min} = 0.8 KuPu, K_{d \max} = 0.15 KuPu \tag{9}$$

4.1.3 Indirect Field Oriented Control (IFOC)

The principle of indirect field-oriented control system of an induction motor is that the d-q coordinate's reference frame is locked to the rotor flux vector, this results in a decoupling of the variables so that flux and torque can be separately controlled by stator direct-axis current i_{ds} , and quadrature-axis current i_{qs} , respectively, like in the separately excited dc machine. To perform the alignment on a reference frame revolving with the rotor flux requires information on the modulus and position of the rotor flux [25].

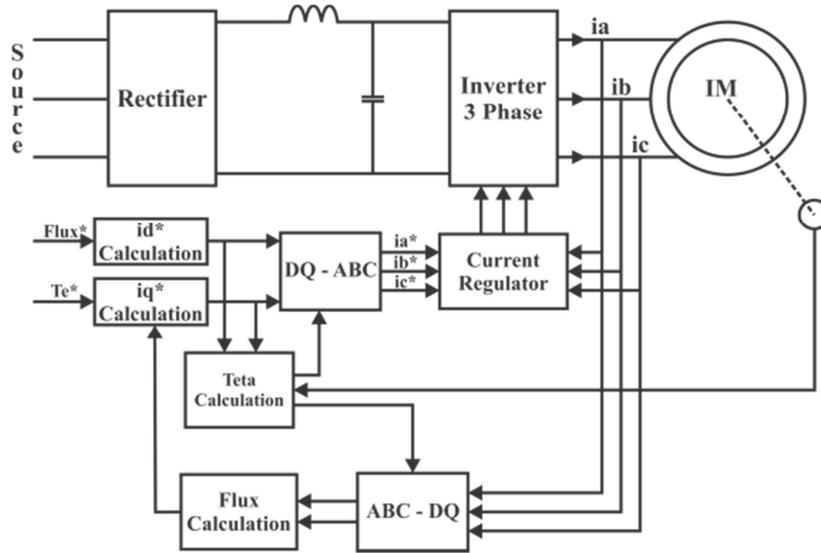


Figure 6. Block of diagram IFOC for Induction Motor

Rotor flux and torque can be separately controlled by stator direct-axis current (i_{ds}) and quadrature-axis currents (i_{qs}) in sequence. Large quadratureaxis current reference (i_{qs}^*) can be calculated by reference torque T_e^* using the following equation:

$$i_{qs}^* = \frac{2}{3} * \frac{2}{P} * \frac{L_r}{L_m} * \frac{T_e^*}{\lambda_r^*} \tag{10}$$

L_r is the rotor inductance, L_m is the mutual inductance and λ_r is the flux linkage rotor estimation which is derived from this equation:

$$\lambda_r = \frac{L_m i_{ds}}{1 + \tau_r s} \tag{11}$$

$\tau_r = \frac{L_r}{R_r}$ is the time constants of rotor. The number of direct-axis stator current reference i_{qs}^* is based on the flux reference input λ_r^* as follow:

$$i_{ds}^* = \frac{\lambda_r^*}{L_m} \tag{12}$$

The angle of flux rotor θ_e for coordinate transformation which is derived from rotation speed of rotor ω_m and slip speed ω_{sl} calculation as follow:

$$\theta_e = \int(\omega_m + \omega_{sl}) dt \quad (13)$$

Slip speed is calculated from stator current reference i_{qs}^* with this following motor parameter:

$$\omega_{sl} = \frac{L_m}{\lambda_r^*} * \frac{R_r}{L_r} * i_{qs}^* \quad (14)$$

Reference current i_{qs}^* converted into a reference-phase flow i_{as}^* , i_{bs}^* , i_{cs}^* using the following equation (10) which will be the input current regulator. Then the flow regulator will process the reference phase current into a signal which triggers will control the inverter.

$$\begin{bmatrix} i_{a^*} \\ i_{b^*} \\ i_{c^*} \end{bmatrix} = \begin{bmatrix} \cos\theta & -\sin\theta \\ (-\frac{1}{2}\cos\theta + \frac{\sqrt{3}}{2}\sin\theta) & (\frac{1}{2}\sin\theta + \frac{\sqrt{3}}{2}\cos\theta) \\ (-\frac{1}{2}\cos\theta - \frac{\sqrt{3}}{2}\sin\theta) & (\frac{1}{2}\sin\theta - \frac{\sqrt{3}}{2}\cos\theta) \end{bmatrix} \begin{bmatrix} i_{d^*} \\ i_{q^*} \end{bmatrix} \quad (15)$$

4.2 Speed Control for three phase induction motor

4.2.1 Implementation modelling IFOC without Speed Control

Based on block of diagram in Fig. 9, it is known by using IFOC method, flux and torque can be controlled separately. Flux will affect field current (i_{ds}^*) and torque will affect torque current (i_{qs}^*). In this work, reference torque (T_e^*) is given fixed value, while reference flux is got from block control output FGS-PID. Then i_{ds}^* and i_{qs}^* are used for the calculation of Control Block of IFOC. The current sensor is used to know the motor current that is also used as calculation of IFOC block control. Output of IFOC block control is converted to be current i_{a^*} , i_{b^*} , i_{c^*} as input current regulator. Then, it will be processed to be a trigger signal that is used to control inverter as motor drive. Speed sensor is used to calculate the theta (θ) at coordinate system (direct axis – quadrature axis) that is used at IFOC block control, and also used for monitoring actual motor speed. Then, it is compared with speed reference so that it gets error value that is processed by PID controller as motor speed control to get speed reference.

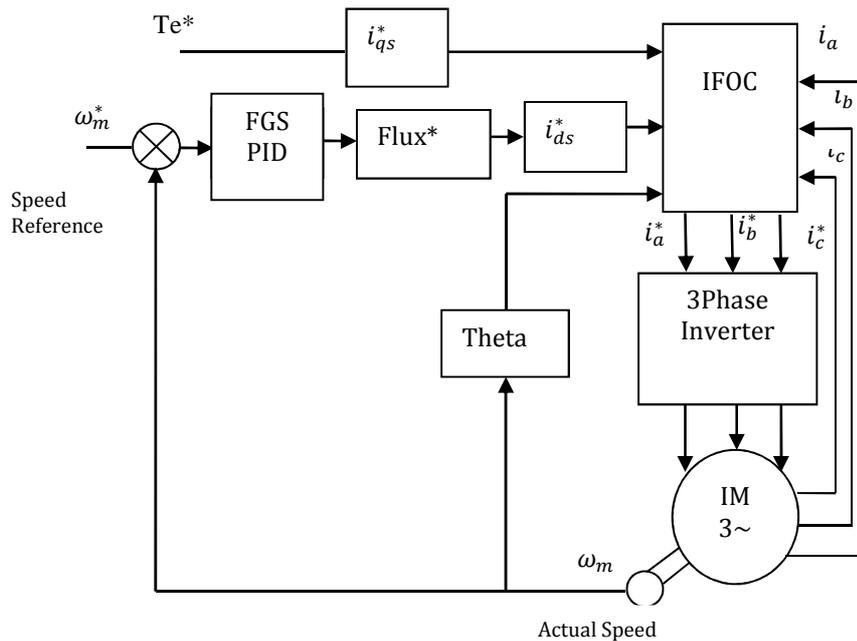


Figure 7. Block diagram of design system

In this paper proposed simulation model of three-phase induction motor with the implementation of Indirect Field Oriented Control (IFOC) system. Parameter of three-phase induction motors that was used in this simulation:

Table 5. Specification of induction motor

No	Motor Parameter	Specification
1	Voltage	400 volt
2	Power	7.5 kw
3	Frequency	50 Hz
4	Speed	1440 Rpm
5	Rotor Type	Squirrel Cage
6	Rotor Resistance	0.7402Ω
7	Stator Resistance	0.7384Ω
8	Rotor Inductance	0.003045H
9	Stator Inductance	0.003045H
10	Mutual Inductance	0.1241H
11	Pole	2
12	Inertia	0.0343Kg

The system IFOC the transformation stationer frame into rotational frame using *Clark* and *Park* Transformation. *Clark* transformation is used to modify three-phase stationary (i_a, i_b, i_c) to be two-phase stationary (i_α, i_β). While, *Park* Transformation modify two-phase stationary to the two phase rotational (i_d, i_q) that was illustrated in Fig. 10.

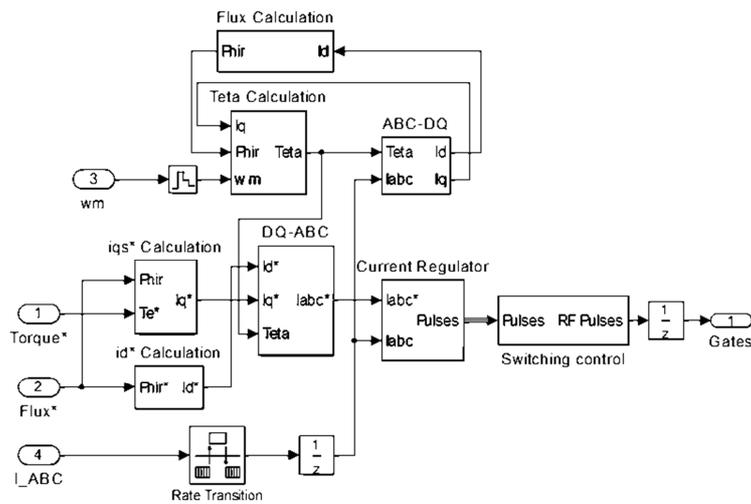


Figure 8. Model of Indirect Field Oriented Control (IFOC)

4.2.1 Design of Fuzzy Gain Scheduling PID

The design of Fuzzy scheduler for FGS-PID using two input values, those are error value and delta error value. The output from the result of scheduler fuzzy is also used to this system based on gain value as the PID control basic calculation. Gain value is determined by scheduling process which can be used to obtain the best and the compatible gain from the operating condition. Scheduling system is also used to determine gain value when there is modification parameter in control system. Fuzzy gain scheduler model of this system is illustrated in Fig.9.

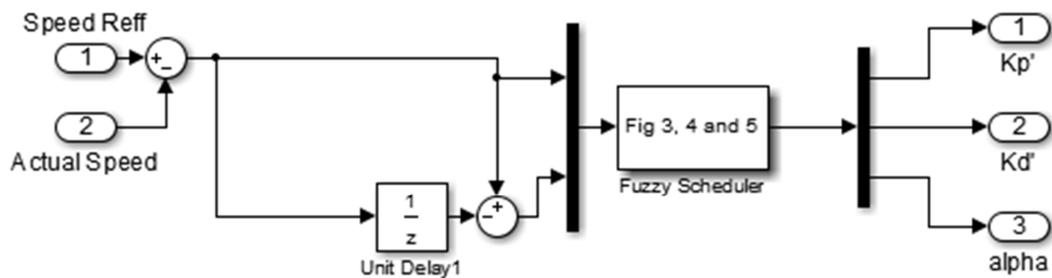


Figure 9. Block of diagram fuzzy gain scheduler

The modification parameter or disturbance which is occurred in control system can be caused transient condition and required addition time to repair the performance from the control system in getting suitable result with setpoint. This condition is influenced with the value of gain which isn't suitable to the PID system and also reduce its performance. Using the compatible gain based on scheduling system can be repaired the response from the output of control system which is still suitable with expected result although it has modification parameters.

5. EXPERIMENT RESULT AND ANALYSIS

5.1 Simulation Result IFOC without Speed Control

The simulation system of IFOC without speed control of three-phase induction motor using IFOC, was depicted in Fig. 10.

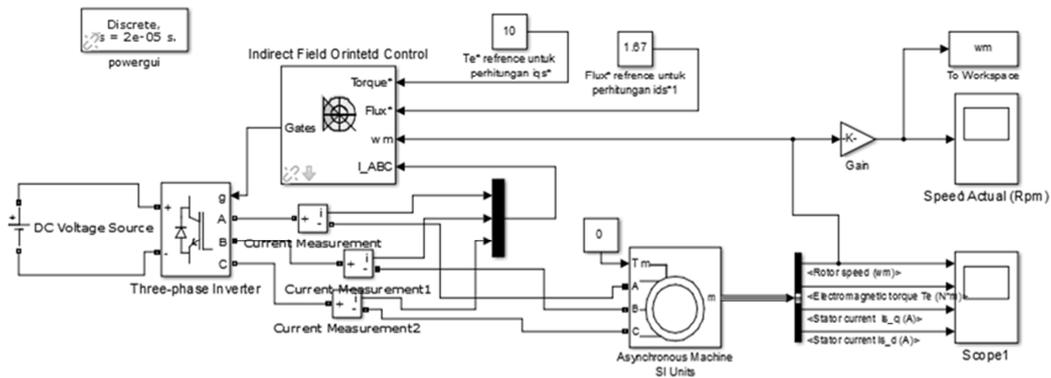


Figure 10. Simulationspeed control of three phase induction motor using IFOC

The output of response speed control using IFOC can be got speed motor in 350 Rpm, 400 Rpm, and 450 Rpm that was illustrated in the following below:.

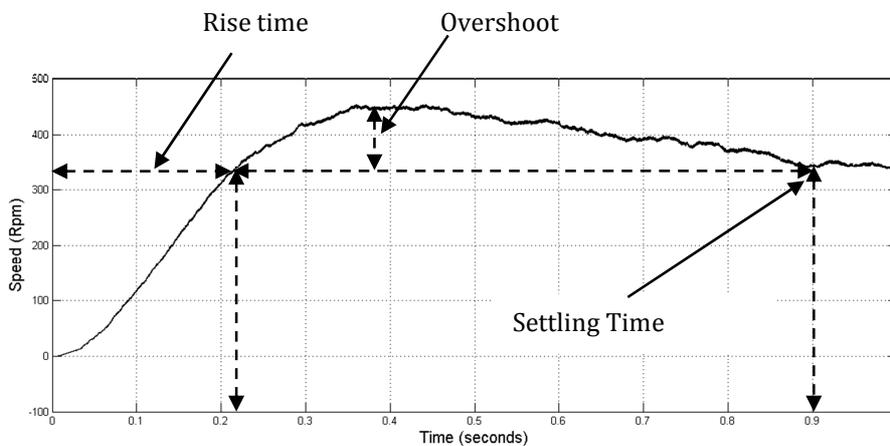


Figure 11. Simulation result speed control with IFOC on the speed motor 350 Rpm

The simulation result (Fig.11) can see the output response system. The rise time value to get speed in 350 Rpm was 0.23 second. The maximum overshoot is 28 %, and time settling 0.89 second before steady speed condition.

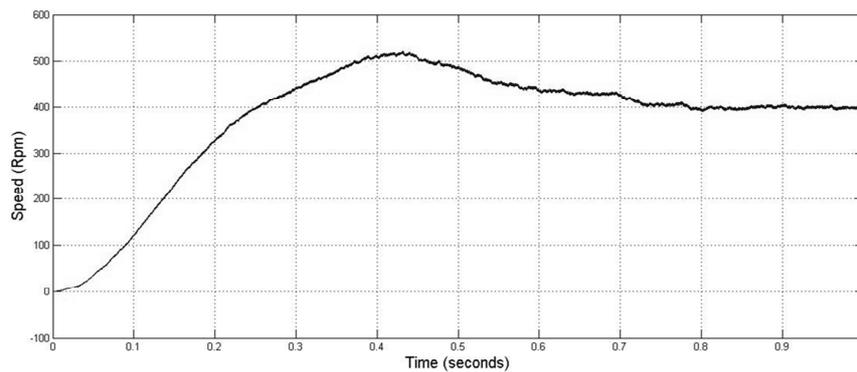


Figure 12.Simulation result speed control with IFOC on the speed motor 400 Rpm

While, the number of rise time to get speed 400 Rpm was needed 0.256 second that has maximum overshoot 29 %, and time settling 0.74 second before condition steady speed, depicted in Fig.12.

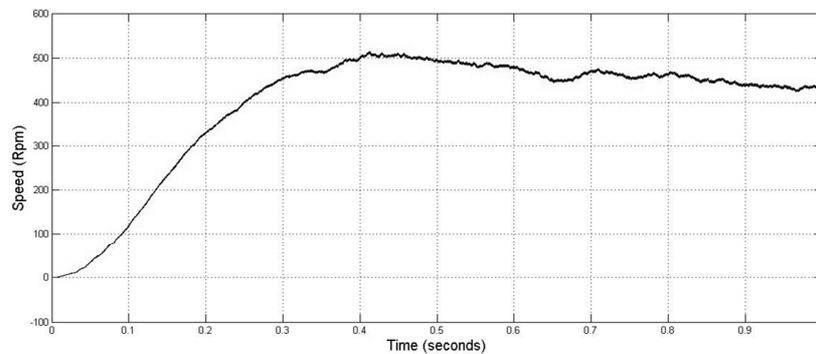


Figure 13.Simulation result speed control with IFOC on the speed motor 450 Rpm

In Fig.13 speed 450 Rpm was needed 0.23 second rise time, 28 % maximum overshoot, and time settling 0.93 second before condition steady speed.

5.2 Simulation Result IFOC with Speed Control FGS-PID

The Fuzzy gain scheduling –PID (FGS-PID) have a structure similar to ideal PID controllers, but their parameters are adapted online based parameter estimation and prediction when there was modification parameter on control process. FGS-PID will perform the process scheduling on the gain that most affect the performance of PID control when there is a modification parameter so as to maintain optimum control response. Fuzzy Logic will perform online tuning to obtain a suitable the gain in accordance with the prescribed range without having to change the gain-gain others. The simulation of IFOC that used speed control FGS-PID for three-phase induction motor, illustrated in Fig. 14.

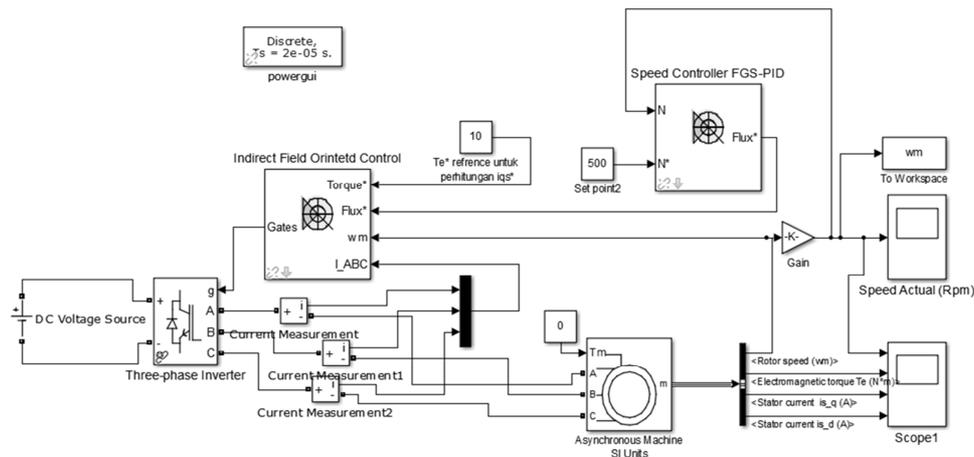


Figure 14.Simulation of IFOC using speed control FGS-PID

In Fig. 15, showsthe diagram block of speed control FGS-PID for three-phase induction motor based on IFOC.

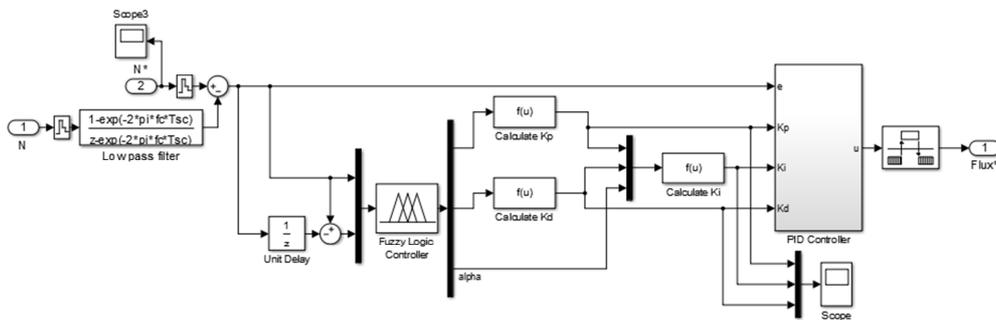


Figure 15.Block of Speed Control IFOC using FGS-PID

The proposed system is tested by dynamic of speed or position modification from setpoint (reference speed) with 0 seconds to 0.01 seconds sampling time. The first condition: we assumed 300 Rpm setpoint, and after the simulation is running at 0.05 seconds in steady state condition, will be increased the setpoint up to 600 Rpm and 0.1 seconds steady state condition. The maximum set point limitation is based on operation fields from scheduling which is 1000 Rpm. The simulation results is observed and analyzed the performance of induction motor in transient condition involve rise time, overshoot, undershoot and settling time.

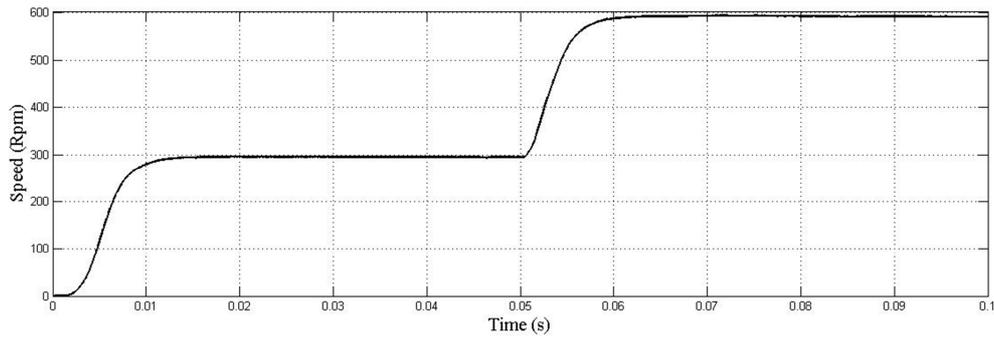


Figure 16.Simulation result FGS-PID at speed modification 300 Rpm – 600 Rpm

The performance result from FGS-PID control for three phase induction motor of IFOC based is using set point variable as shown in Fig.20. The sytem responses can be analyzed or observed with 0.1 seconds sampling time as follows:

Table 6.Result observation transien condition at speed control using FGS-PID

	Speed (Rpm)	
	300	600
Rise time (s)	0.0135	0.0132
Overshoot (%)	0	0
Undershoot (%)	0	0
Settling time (s)	0.014	0.0143

The next condition, we declared 400 Rpm setpoint and 0.05 seconds steady state condition at the runned simulation. It will be reduced up to 200 Rpm setpoint and 0.1 seconds in steady state condition. For the last, the setpoint is set in 150 Rpm and 0.1 seconds steady state condition.

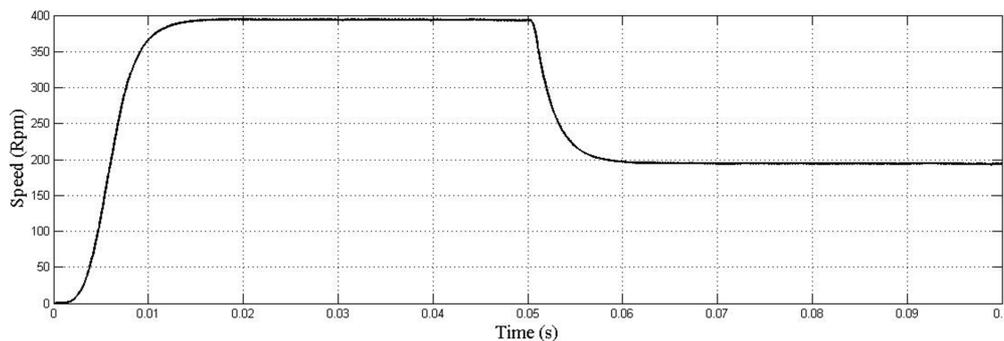


Figure 17.Simulation result FGS-PID at speed modification 400 Rpm – 200 Rpm

The result responses sytem from second condition of FGS-PID can see in Fig.17 and it analyzed or observed show in table 7:

Table 7. Second result observation transien condition using speed control FGS-PID

	Speed (Rpm)	
	400	200
Rise time (s)	0.017	0.0085
Overshoot (%)	0	0
Undershoot (%)	0	0
Settling time (s)	0.017	0.0173

From the observation above is known that FGS-PID control has a better response can be solve the problem in transient condition to get steady state

condition only takes less than 0.01 seconds without getting overshoot and undershoot.

5.3 The comparison proposed FGS-PID with other speed control

FGS-PID control are proposed to be used to improve transient conditions in implementation IFOC for induction motors to achieve steady state when modified parameters. By performing IFOC methods for induction motor can be to modify characteristic nonlinear similarly of DC motor which is expected to control systems designed to obtain optimal results because the process is controlled in linear conditions. Some control used on an induction motor, majority want to get good result to achieve setpoint so ignore the transient condition other. The performance result from the comparison between FGS-PID, PID-Zn and Fuzzy Backstepping for three phase induction motor of IFOC based is using set point variable as shown in Fig.18. The sytem responses can be analyzed and observed with 0.1 seconds sampling time as follows:

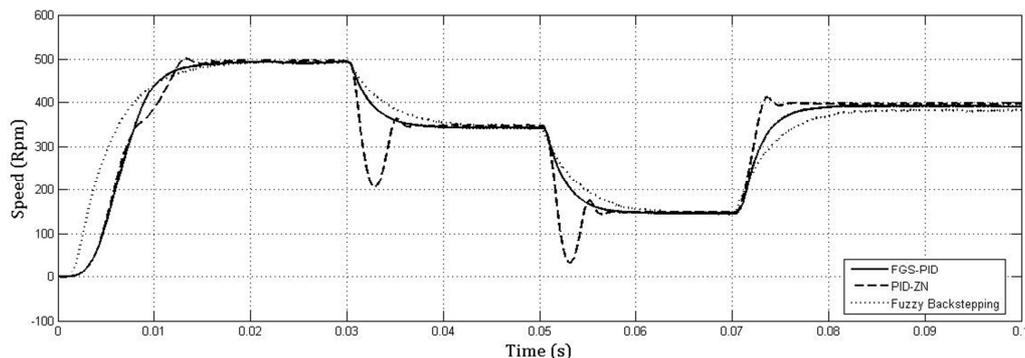


Figure 18. Comparison between FGS-PID, PID-ZN, and Fuzzy Backstepping at speed of dynamic

The comparison result is observed respon induction motor in transient condition for speed of dynamic, shown on the table 8, 9, and 10.

Table 8. The result observation transien condition on speed control FGS-PID

	FGS-PID			
	Speed (Rpm)			
	500	350	150	400
Rise Time (s)	0.015	0.006	0.001	0.0085
Overshoot (%)	0	0	0	0
Undershoot (%)	0	0	0	0
Settling Time (S)	0.0173	0.0010	0.0011	0.0014

Table 9. The result observation transien condition on speed control PID-ZN

	PID-ZN			
	Speed (Rpm)			
	500	350	150	400
Rise Time (s)	0.013	0.0015	0.005	0.0035
Overshoot (%)	0.11	3.42	15.2	0.302
Undershoot (%)	2.04	40.71	76.9	1.56
Settling Time (S)	0.018	0.007	0.0075	0.0095

Table 10. The result observation transien condition on speed control Fuzzy-Backstepping

	Fuzzy-Backstepping			
	Speed (Rpm)			
	500	350	150	400
Rise Time (s)	0.0185	0.0095	0.0093	0.0105
Overshoot (%)	0	0	0	0
Undershoot (%)	0	0	0	0
Settling Time (S)	0.0195	0.0035	0.0014	0.0016

From the comparison result of the control system in Fig. 18, can be observed the transient condition result involved rise time, overshoot undershoot and settling time. The result shows the better performance from the proposed method using FGS-PID in modification parameter which is verified by the result from Table 7-10. The longest time for modification only needs 0.0014 seconds to achieve steady condition without overshoot and undershoot condition. While using PID-ZN take 0.007 seconds to reach steady condition and the Fuzzy-Backstepping need 0.0014 seconds. It proves that the proposed method has better performance in modification parameter.

5.4 Scheduler of parameter gain on PID control

The results of the scheduling gain of PID parameters are presented below:

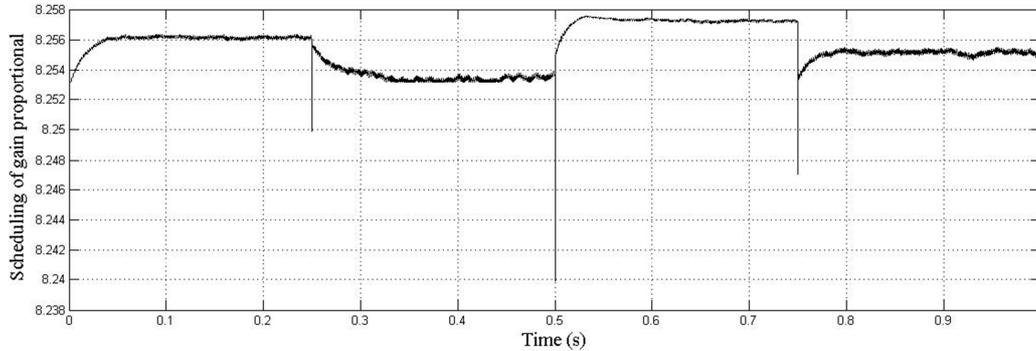


Figure 25.Scheduler of gain proportional for the control of dynamic speed 250 Rpm, 500 Rpm, 100 Rpm, and 300 Rpm

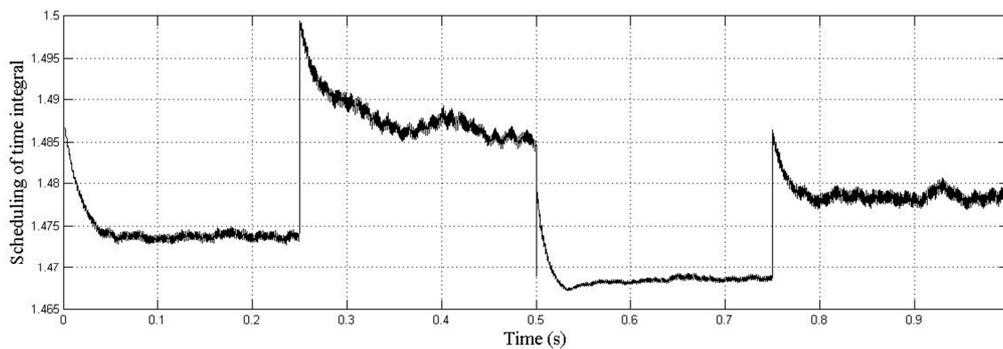


Figure 26.Scheduler of time constant integral for the control of dynamic speed 250 Rpm, 500 Rpm, 100 Rpm, and 300 Rpm

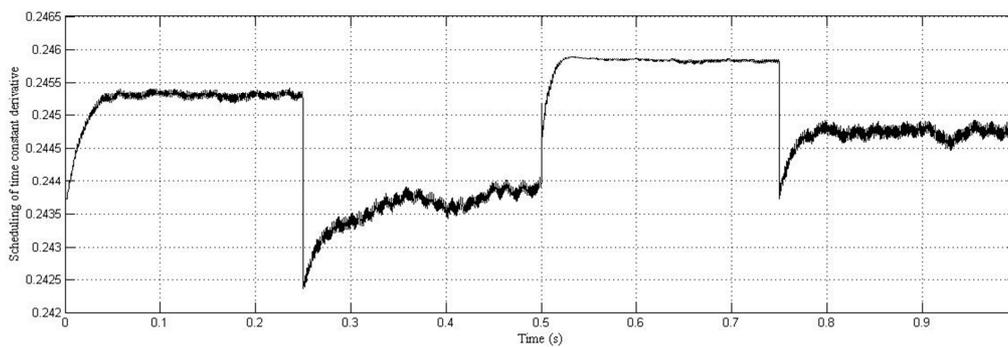


Figure 27.Scheduler of time constant derivative for the control of dynamic speed 250 Rpm, 500 Rpm, 100 Rpm, and 300 Rpm

On the graph in Fig 25, Fig 26, and Fig 27, it can be observed that scheduling gain process will be performed when control process parameter is modified, so it still gets a good result. From the results above with a sampling time of 0-1 second, it is observed on performed scheduling process. At time 0 - 0.25 second with setpoint 250 rpm, then obtained value gain of proportional (Kp) is 8,256, time integral constant (Ti) is at 1.474, and time derivative constant (Td) is 0.2455. When there is a modified setpoint to be 500 rpm at 0.25 - 0.5 seconds, it is performed the scheduling again to get a suitable value. (Kp) is 8.2537, (Ti) is 1.486, and (Td) is 0.2437. And then, when setpoint is 100 Rpm at time 0.5 - 0.75 second, the result of scheduling (Kp) is 8.2577, (Ti) is 1.478, and (Td) is 0.2457. When the last condition, setpoint is 300 Rpm at time 0.75 - 1 second, (Kp) is 8.255, (Ti) is 1.478, and (Td) is 0.24457.

6. CONCLUSION

Design of proposed FGS-PID in the three-phase induction motor speed control using IFOC methods can provide good results. It is verified with testing a reliability of control system on dynamic speed. With this method of observation in transient conditions (involve rise time, overshoot, undershoot, and settling time) it can be known that the performance of the control system is in good condition although the parameters of process control is modified, because it has a fast response below 0.0004 second to achieve a steady state condition without getting overshoot and undershoot. The other advantage of FGS-PID based on IFOC in induction motors is, it can have linearization characteristic of the motor, so it can be easy to control as DC motor. Thus, when getting linear conditions, FGS-PID control can more easily generate optimum performance even though applied to condition of fluctuation.

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